

Numerical simulation in machinised tunnelling

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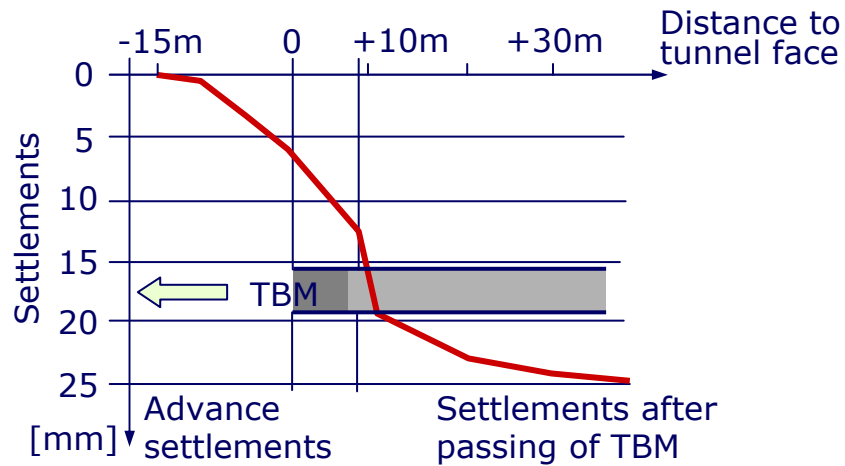
IKT Pipe Jacking Symposium 2007

February 14th, 2007

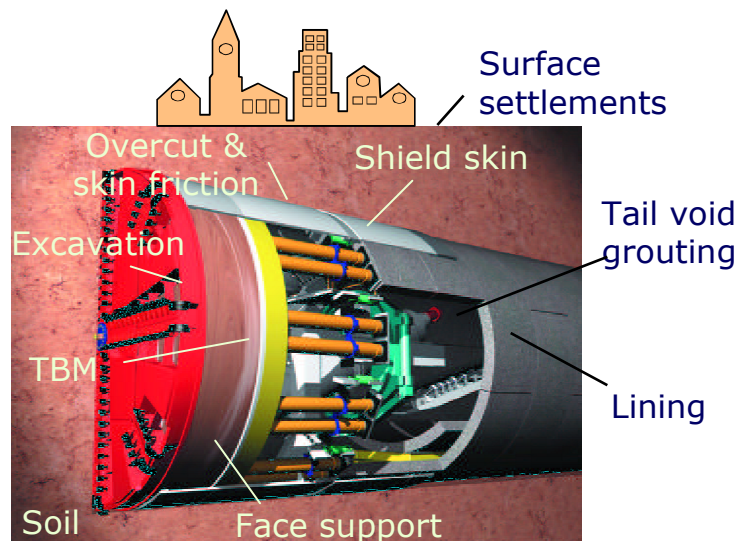
Gelsenkirchen



3D Simulations in TBM tunnelling

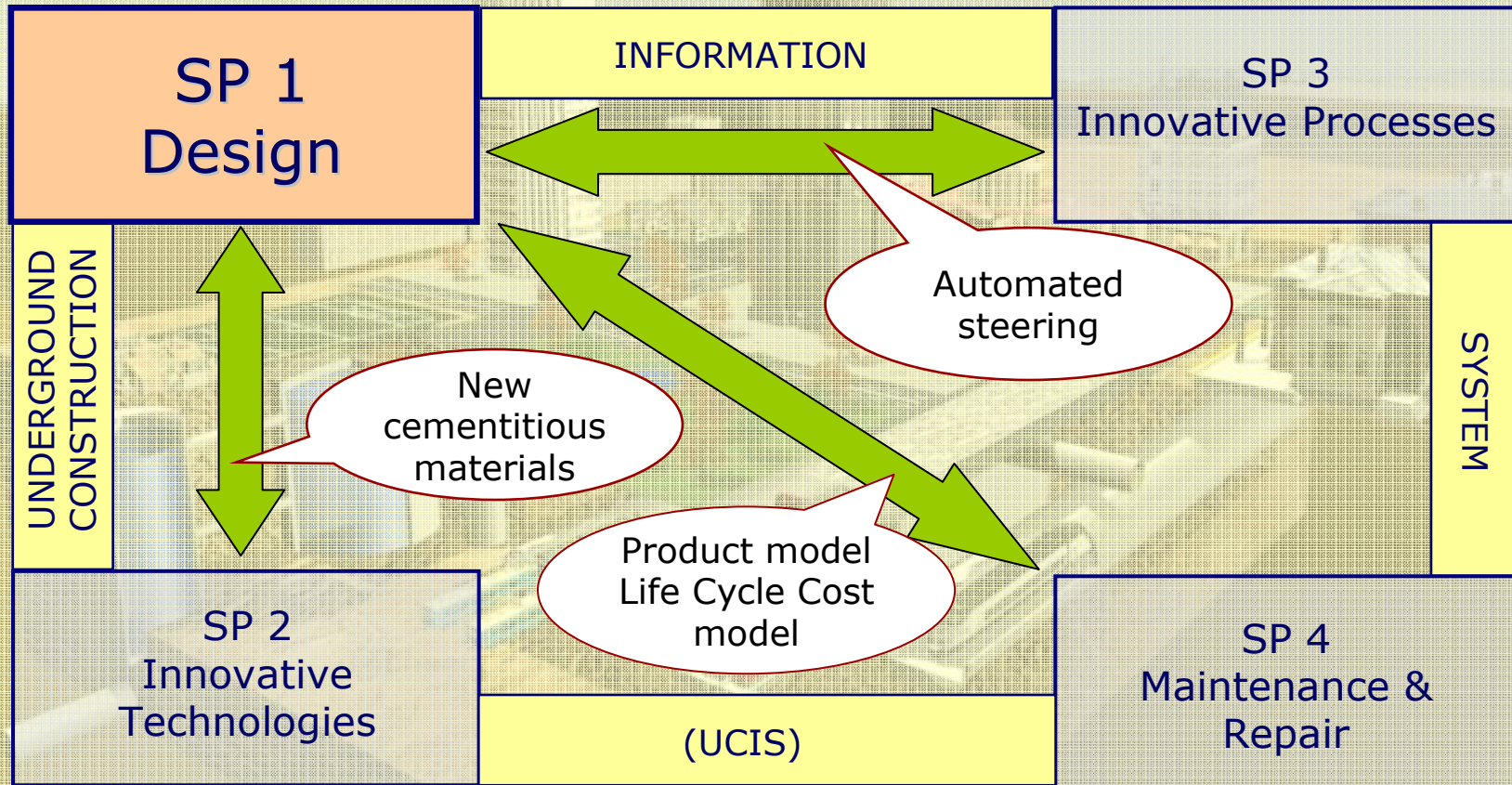


- ✓ Reliable prognoses of settlements (in particular in sensitive urban areas), stresses in tunnel lining etc.
- ✓ Insight into interacting mechanisms between individual components
- ✓ Sensitivity studies: Evaluation of influence of selected parameters
- ✓ Investigation of difficult soil conditions, identification of critical situations, failure of tunnel face
- ✓ Basis for optimization of design of tunnel excavation

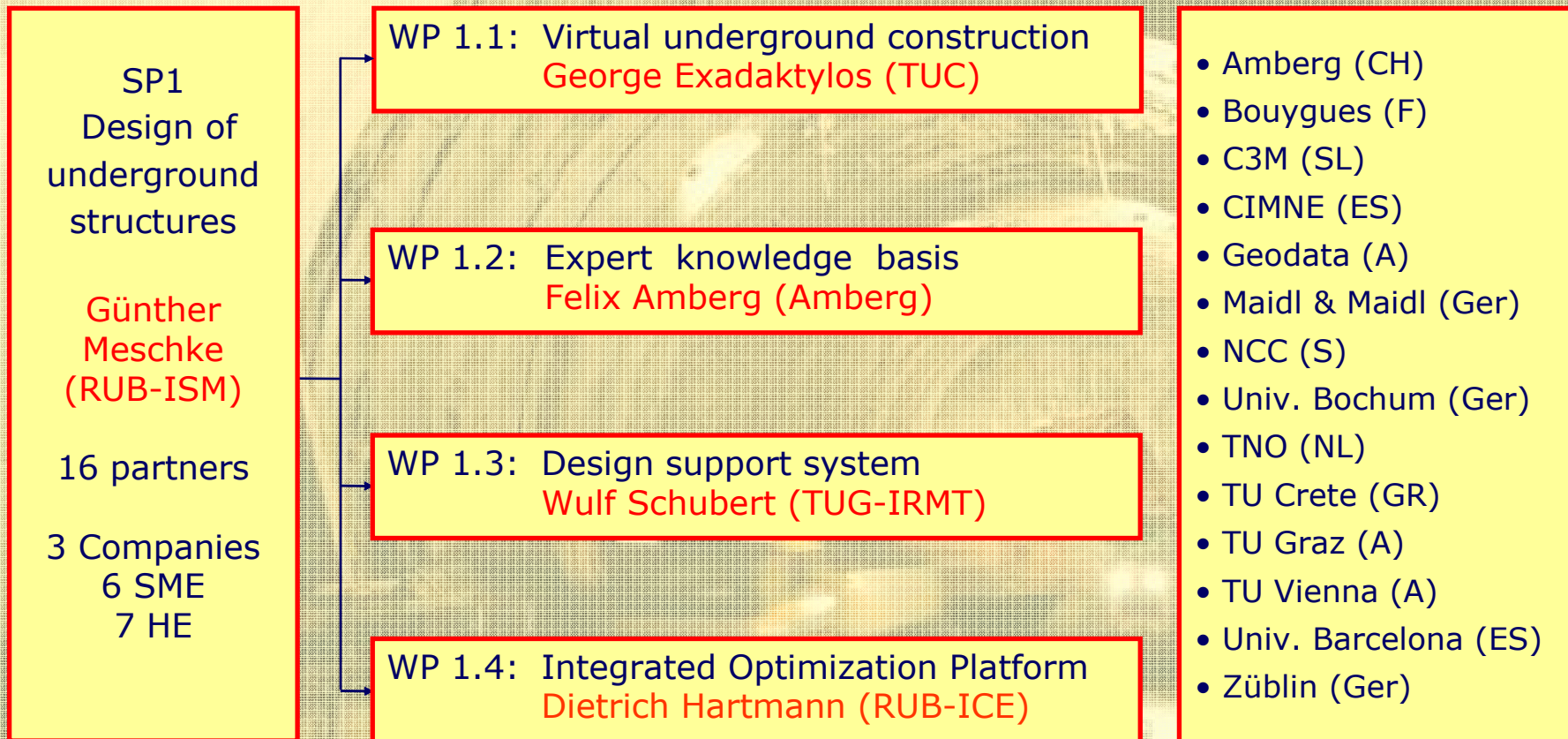


Motivation	Numerical model	Numerical Analyses	Aspects of optimization	Research perspectives
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European Research Initiative TUNCONSTRUCT



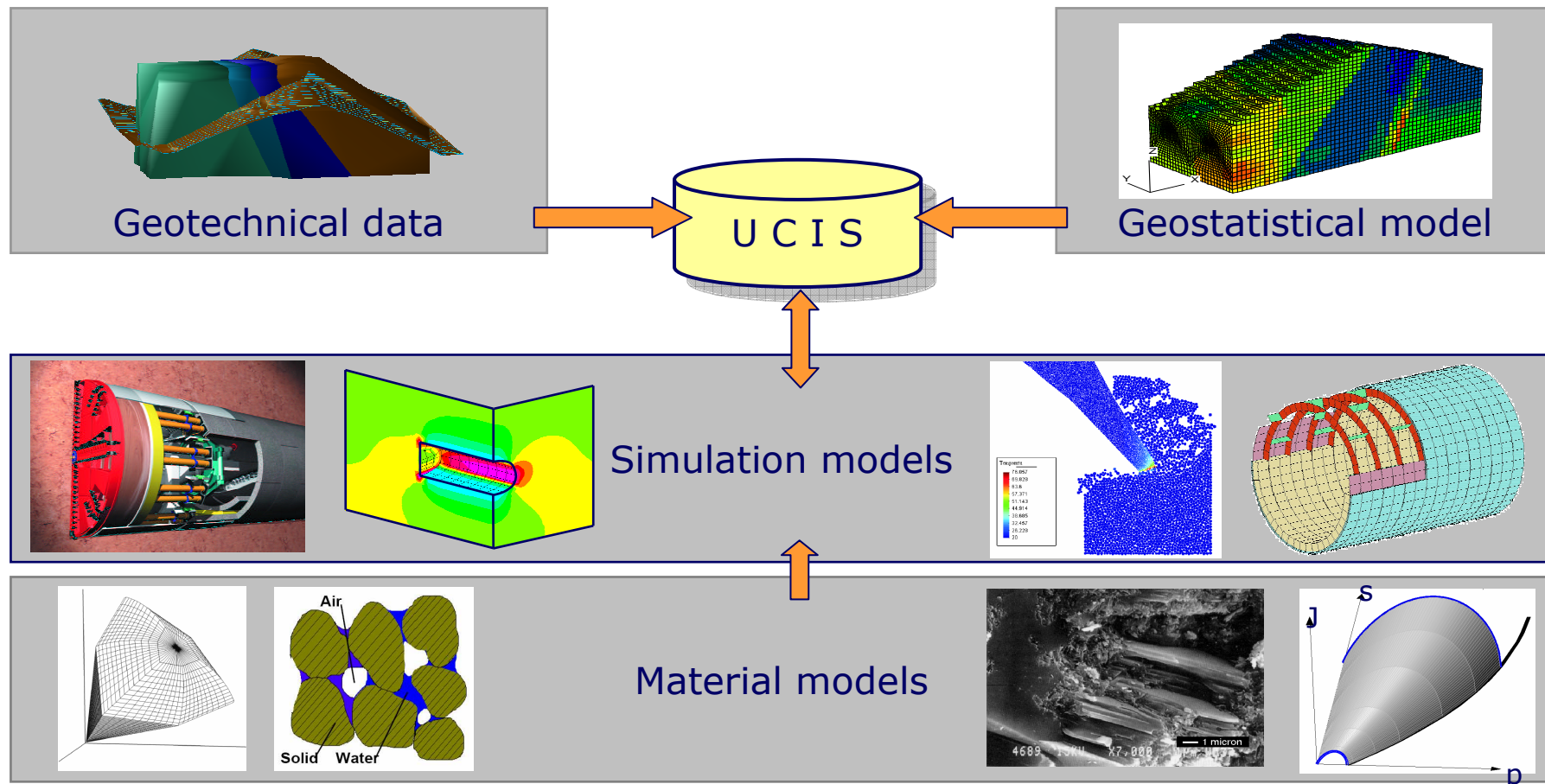
Subproject 1: Design of Underground Construction



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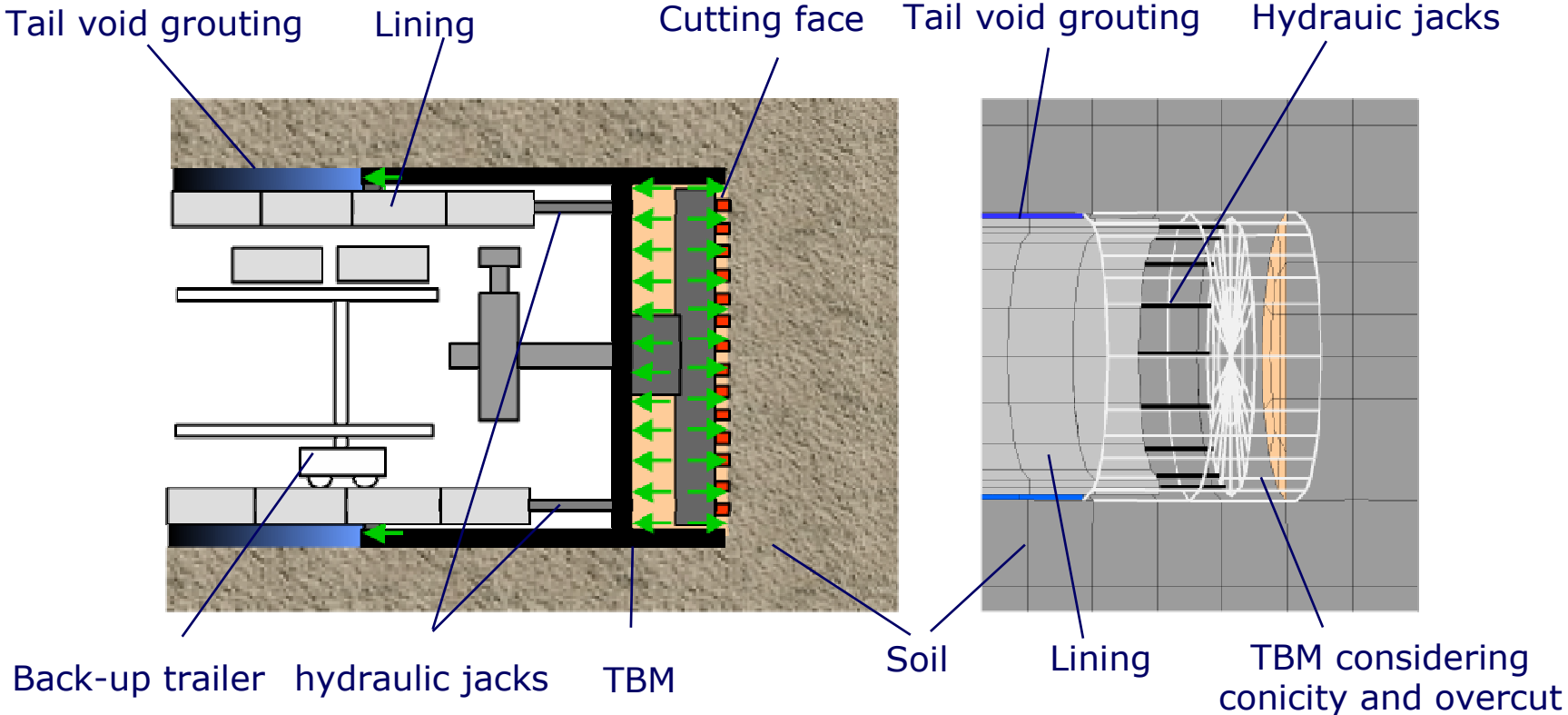
Integrated Concept for Numerical Simulation in Tunnelling



Model components	Fully & partially saturated soil	Tail void grouting	Face support	TBM steering	Simulation procedure
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Construction process

Simulation

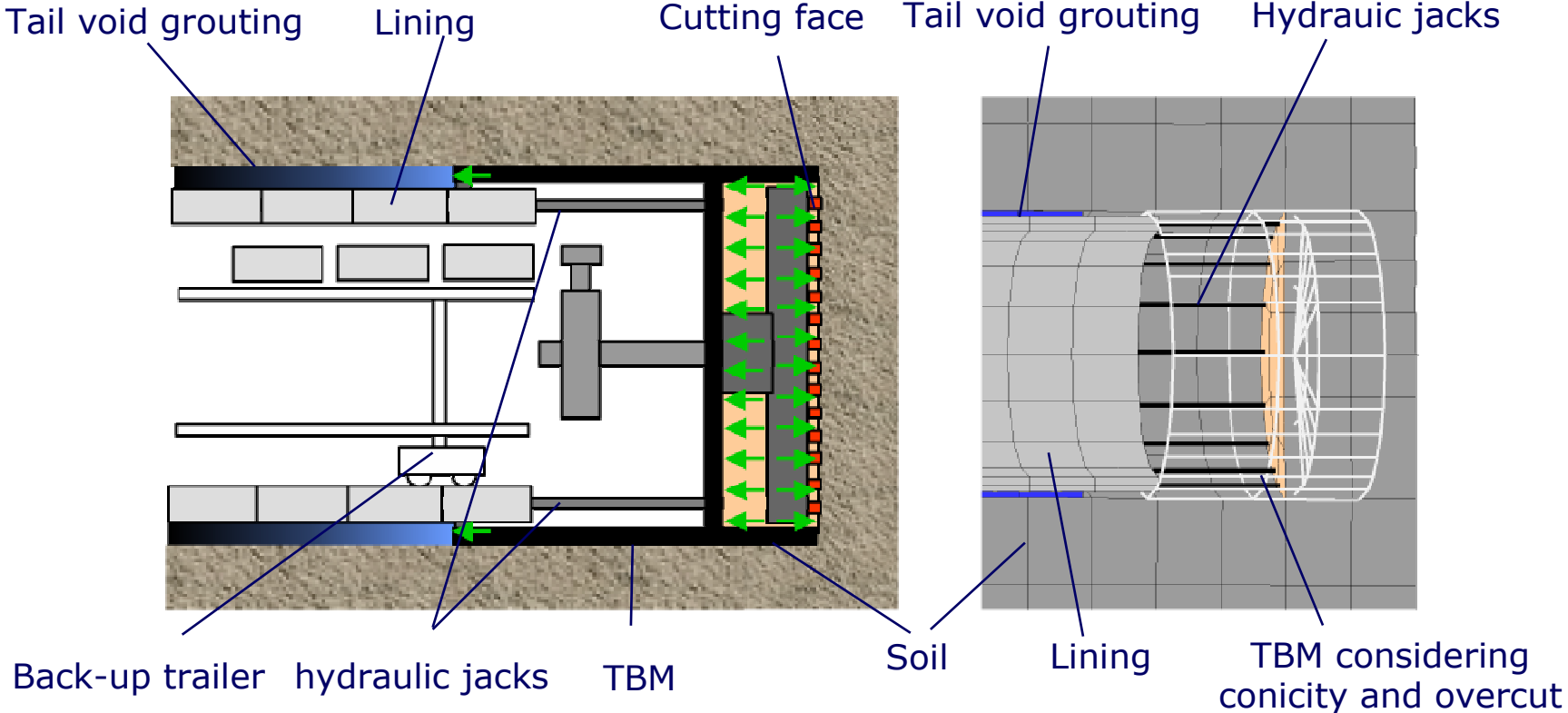


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Construction process

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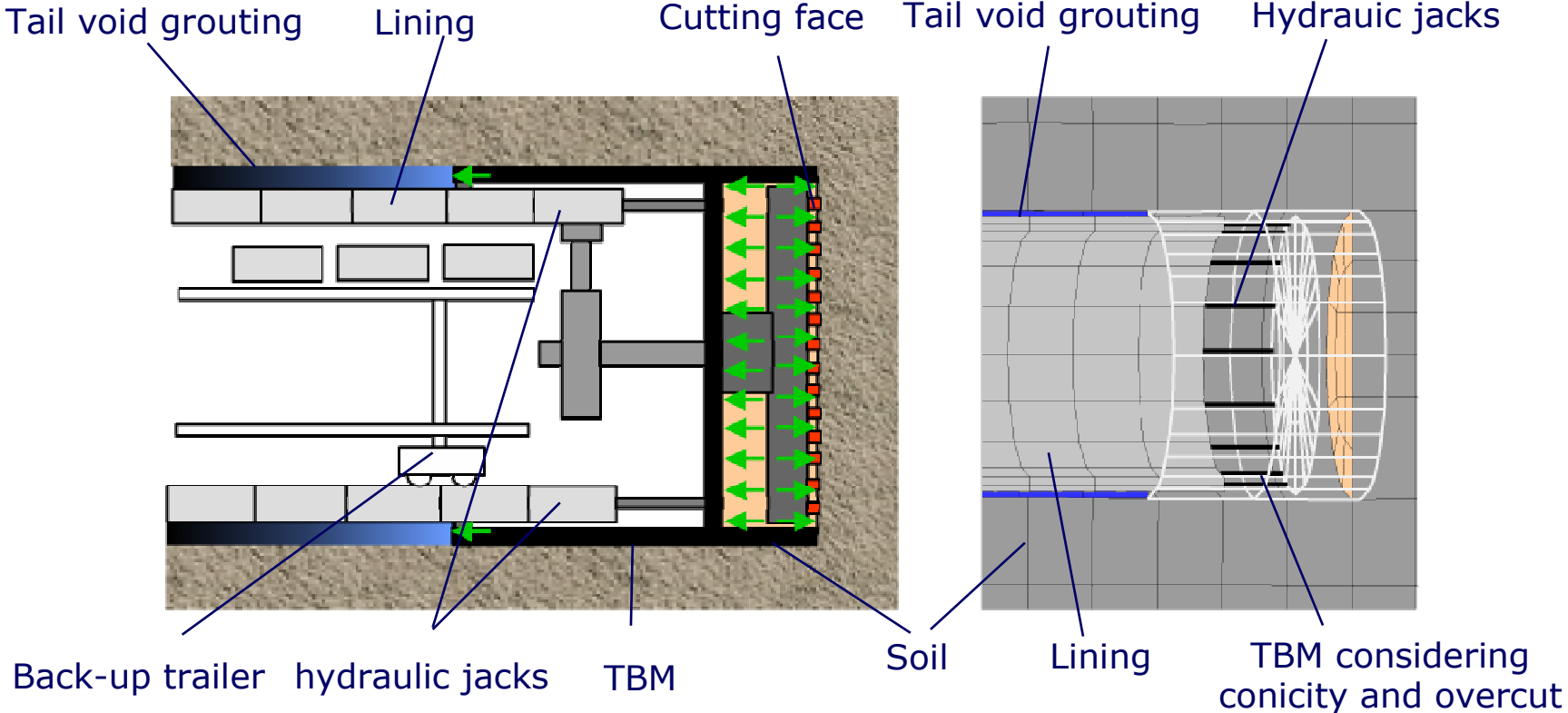


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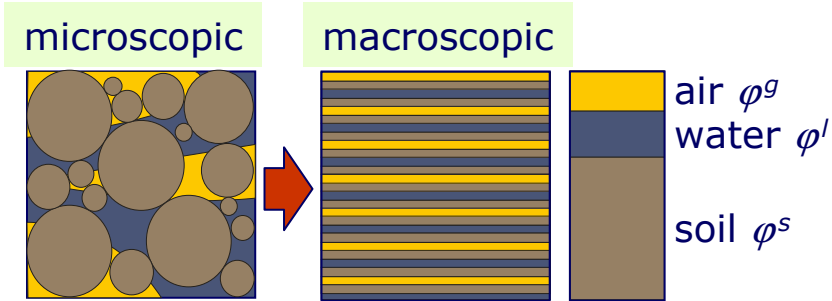
Model components	Fully & partially saturated soil	Tail void grouting	Face support	TBM steering	Simulation procedure
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Construction process

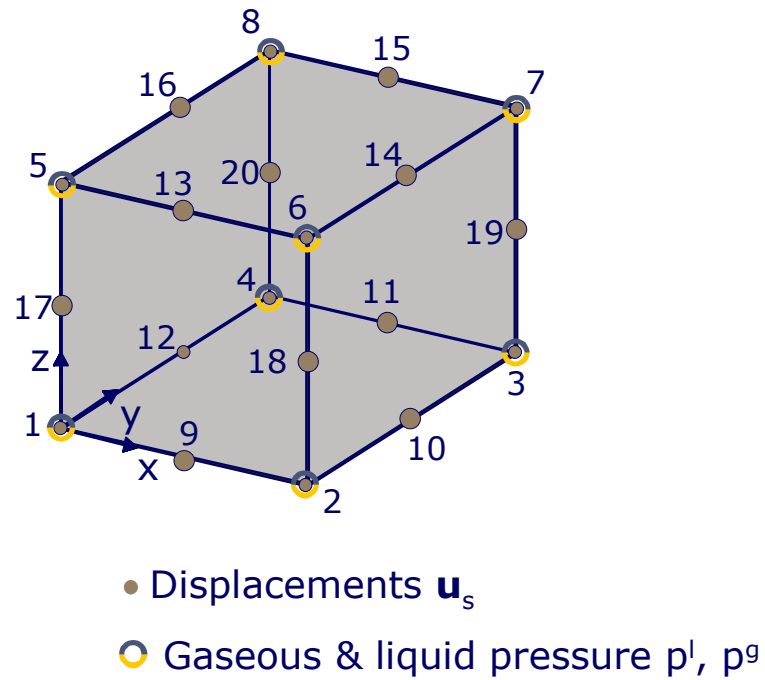
Simulation



Motivation	Numerical model	Numerical Analyses	Aspects of optimization	Ongoing research
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Mixture theory for 3-phase materials



Modelling of partially saturated soils

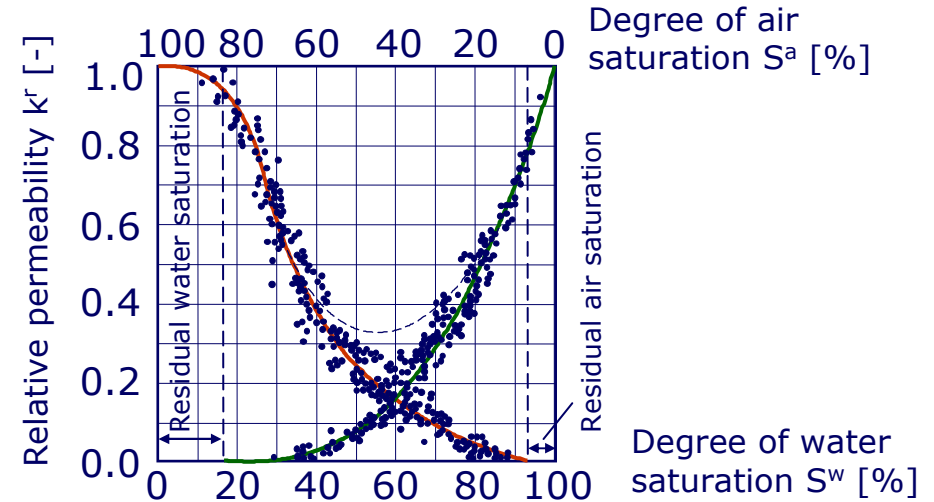
Balance of momentum $\text{div} \boldsymbol{\sigma} + \rho \mathbf{b} = 0$

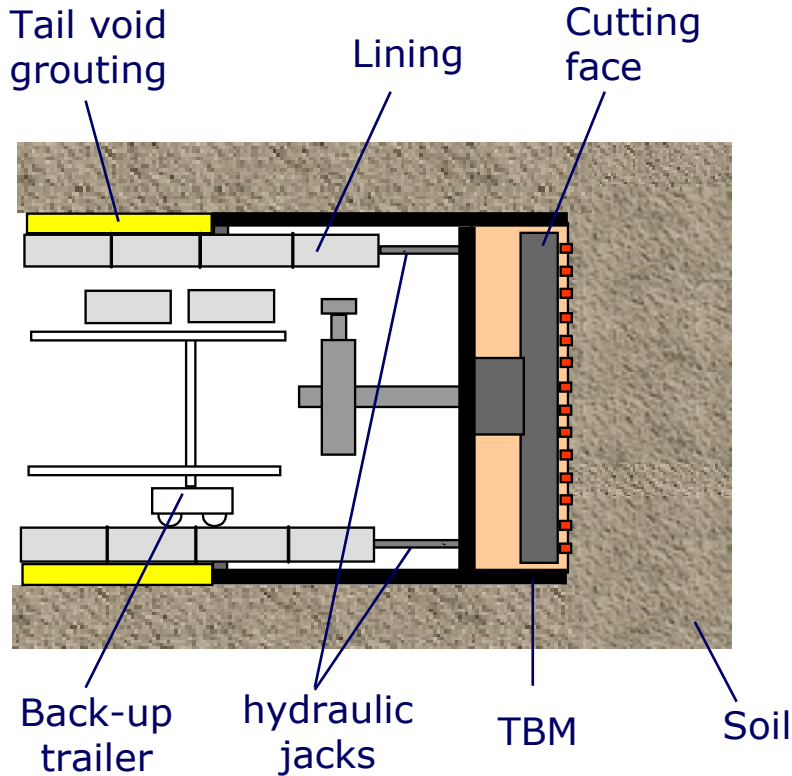
Balance of mass of gaseous phase $\frac{\partial \phi^g \rho^g}{\partial t} + \phi^g \rho^g \text{div} \mathbf{w}^g = 0$

Balance of mass of liquid phase $\frac{\partial \phi^l}{\partial t} + \phi^l \text{div} \mathbf{w}^l = 0$

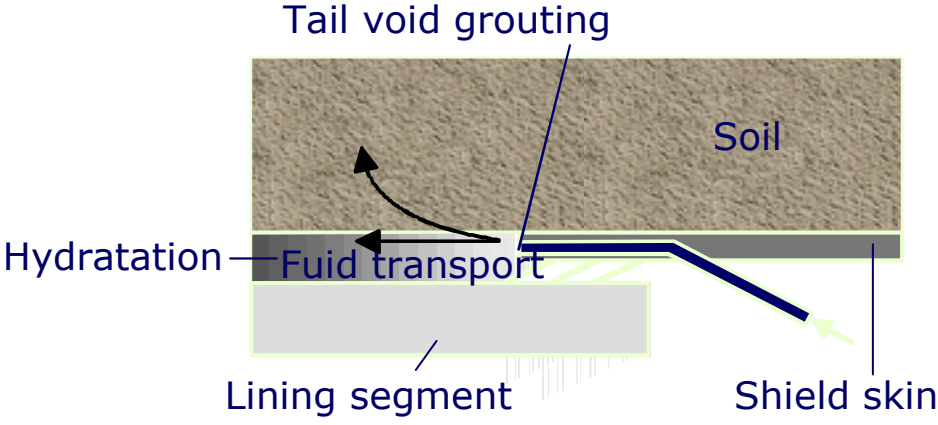
DARCY – law for fluid phases $\mathbf{q}^\beta = \frac{k^\beta}{\mu^\beta} (-\nabla p^\beta + \rho^\beta \mathbf{g})$

Relative permeabilities k^g and k^l according to VAN GENUCHTEN (1985)

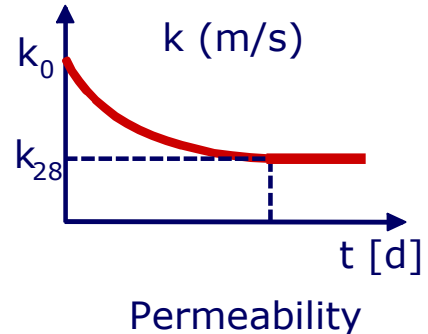
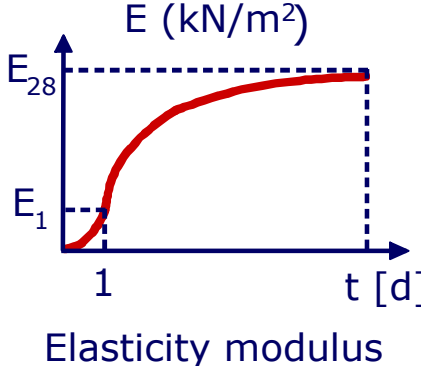
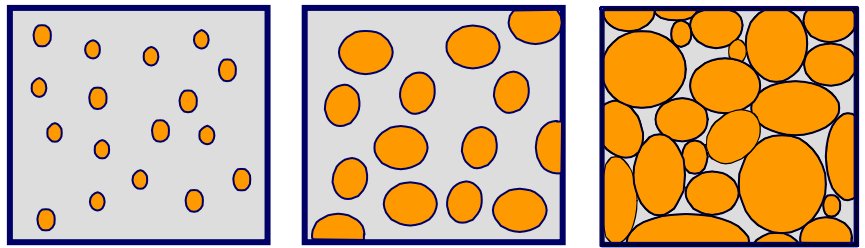




Modelling of tail void grouting

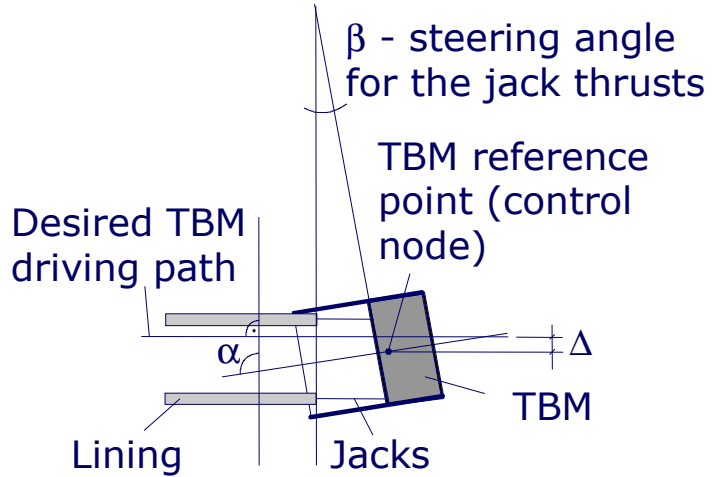
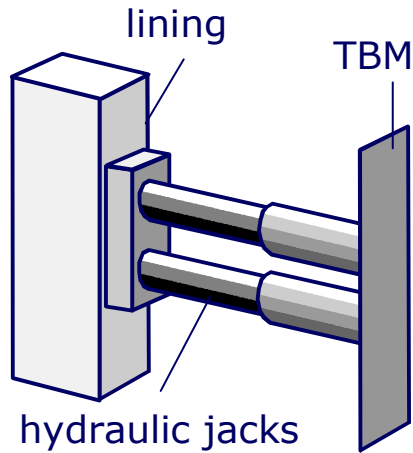


2-phase material with hydration-dependent stiffness and permeability

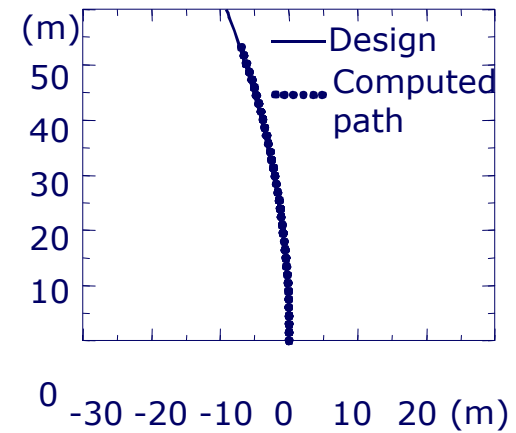
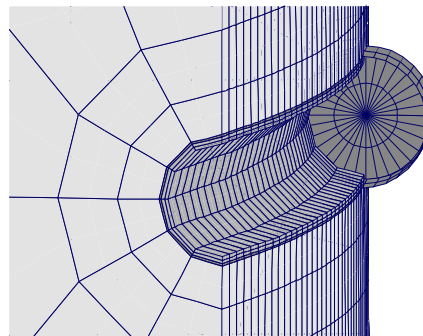
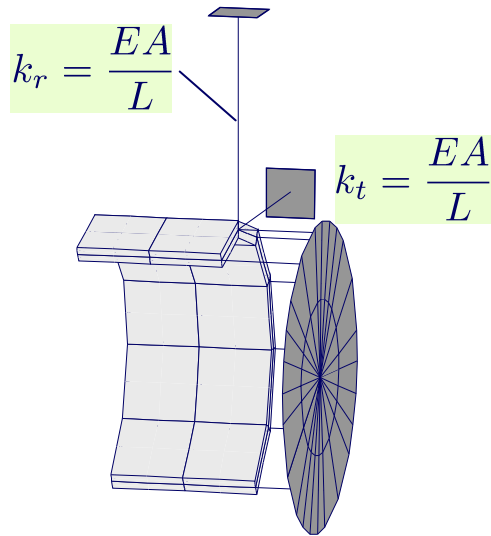


Accounts for interactions between grout and soil

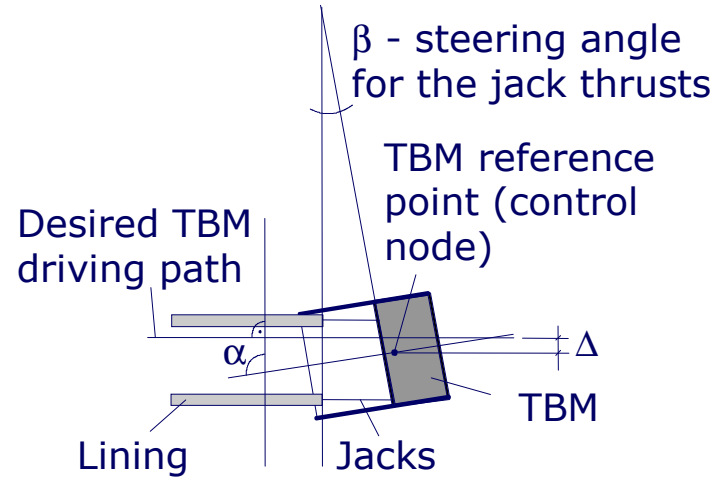
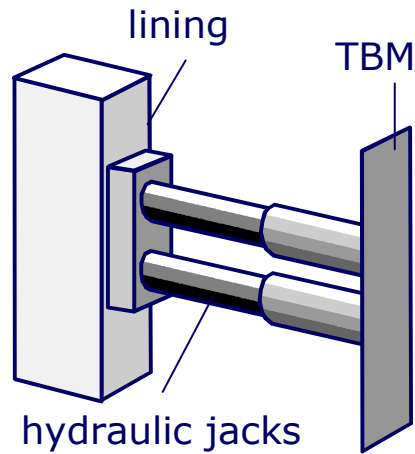
Construction



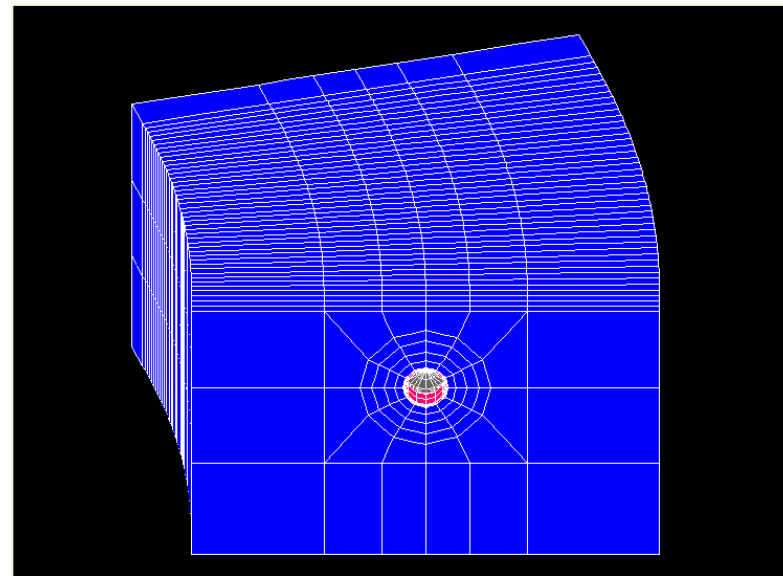
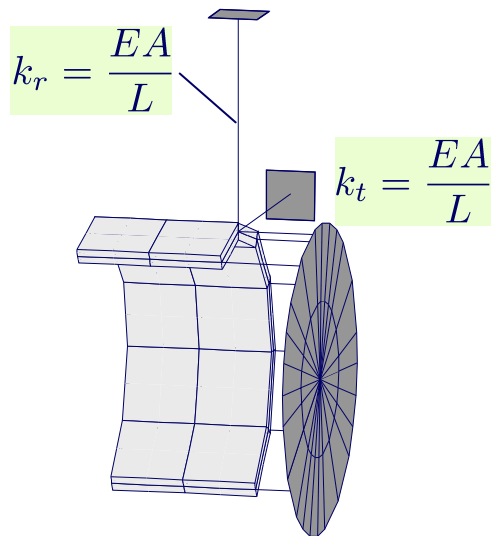
Simulation



Construction

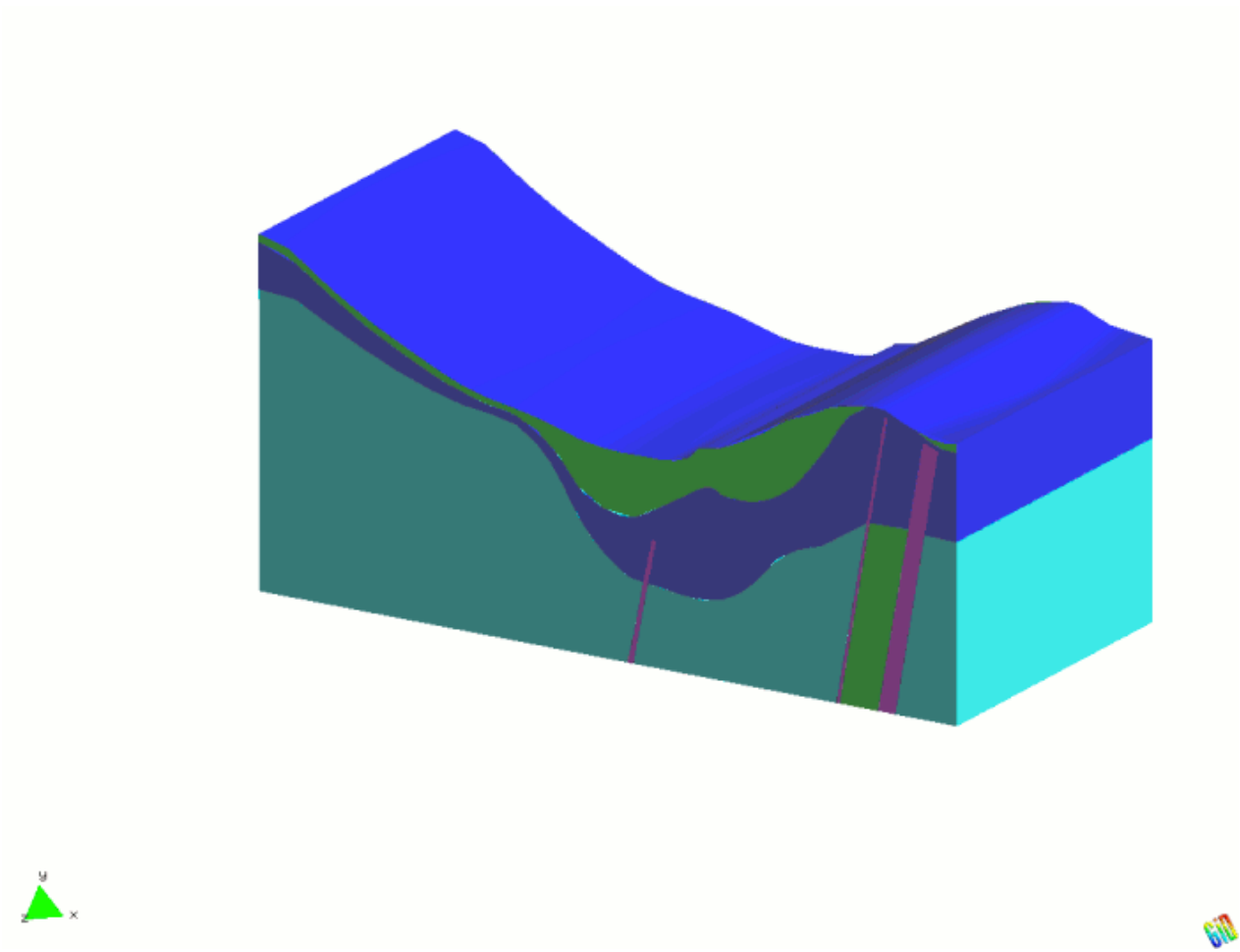


Simulation



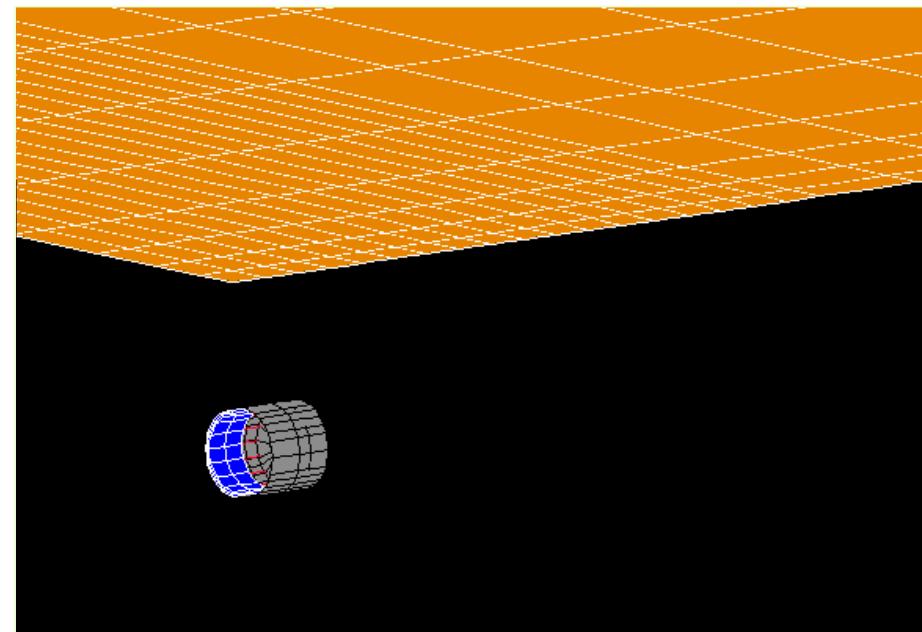
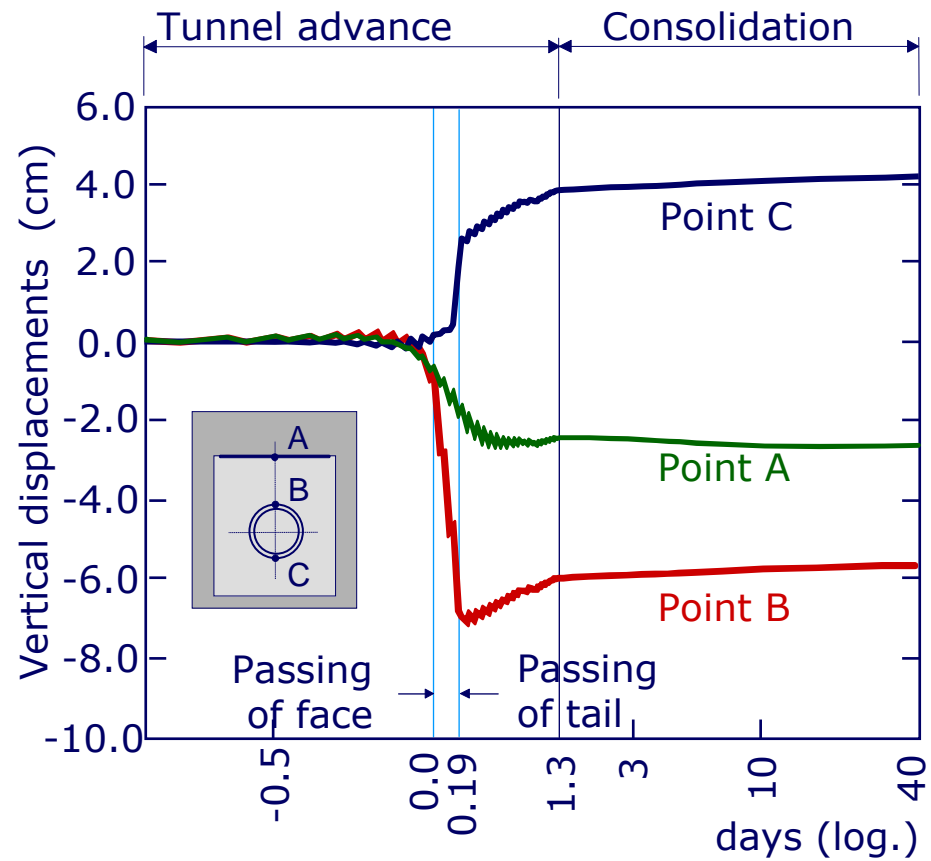
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Integration of geological, geotechnical and simulation model

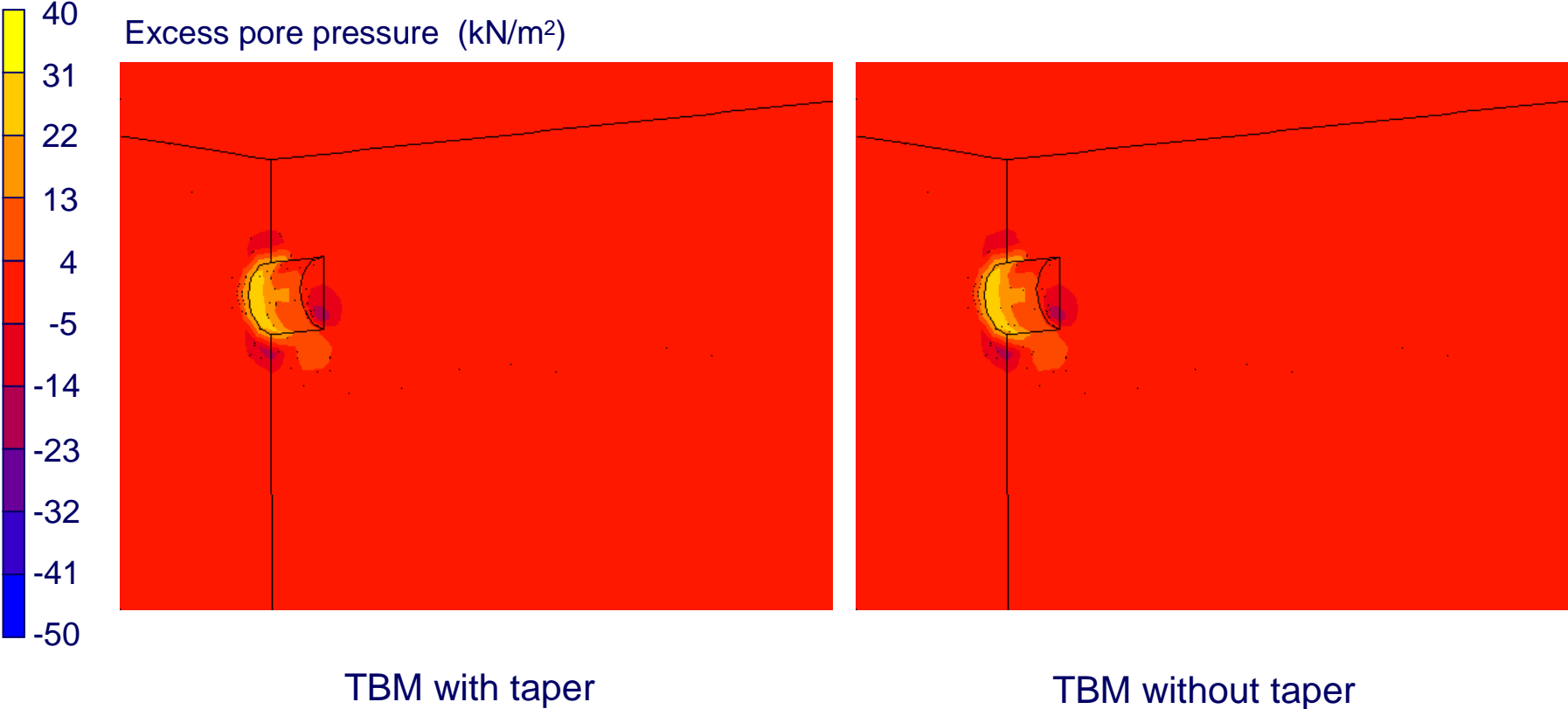


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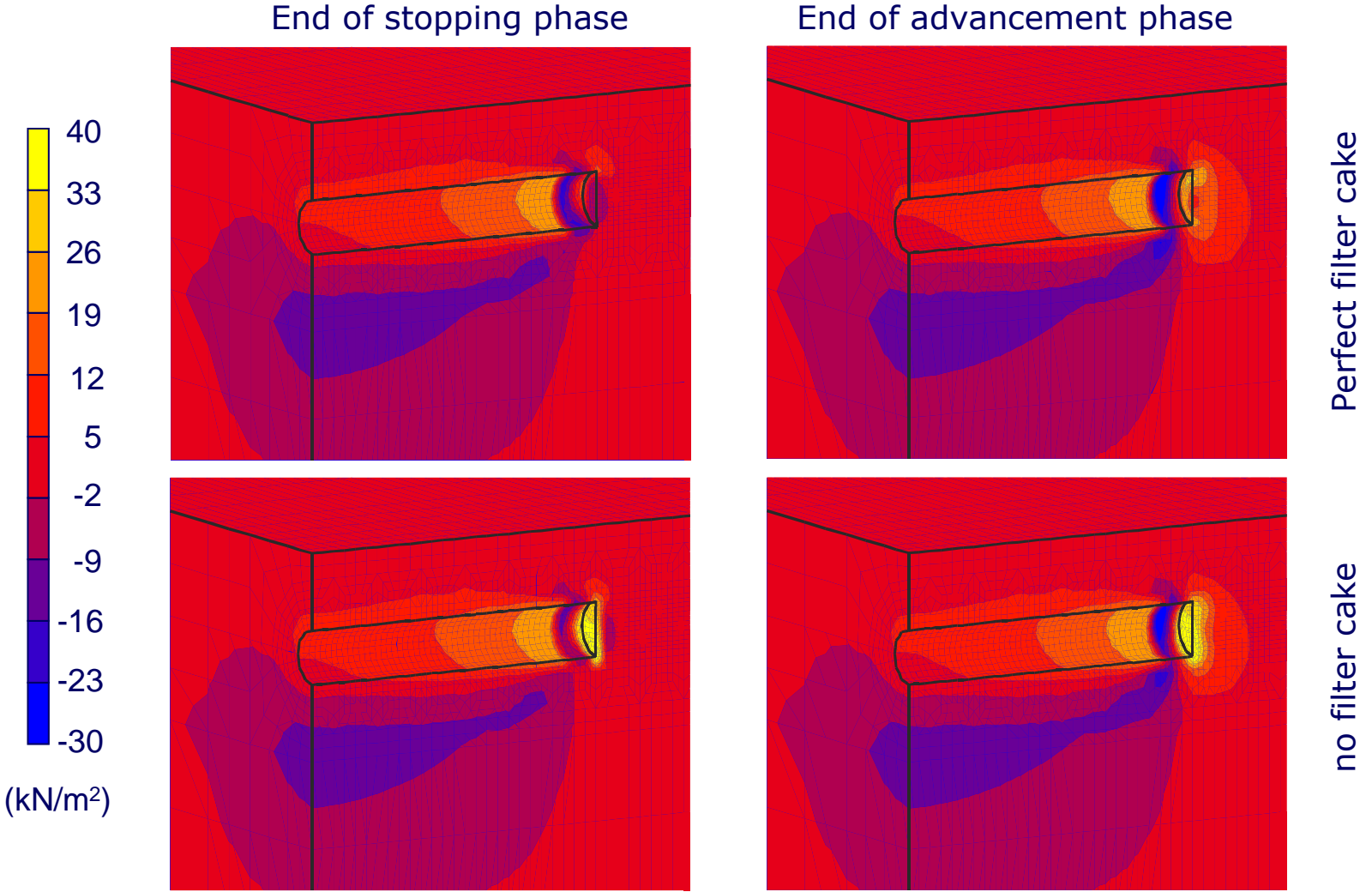
Prognosis of settlements



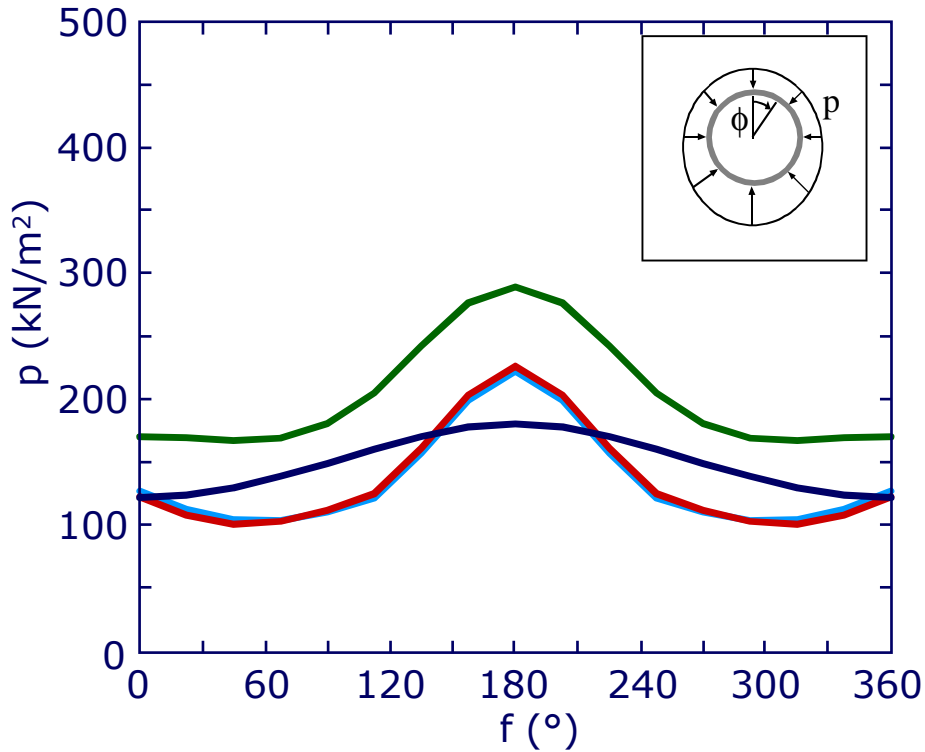
Computed excess pore pressures during the tunnel advance



Computed excess pore pressures during tunnel advance – Influence of filter cake

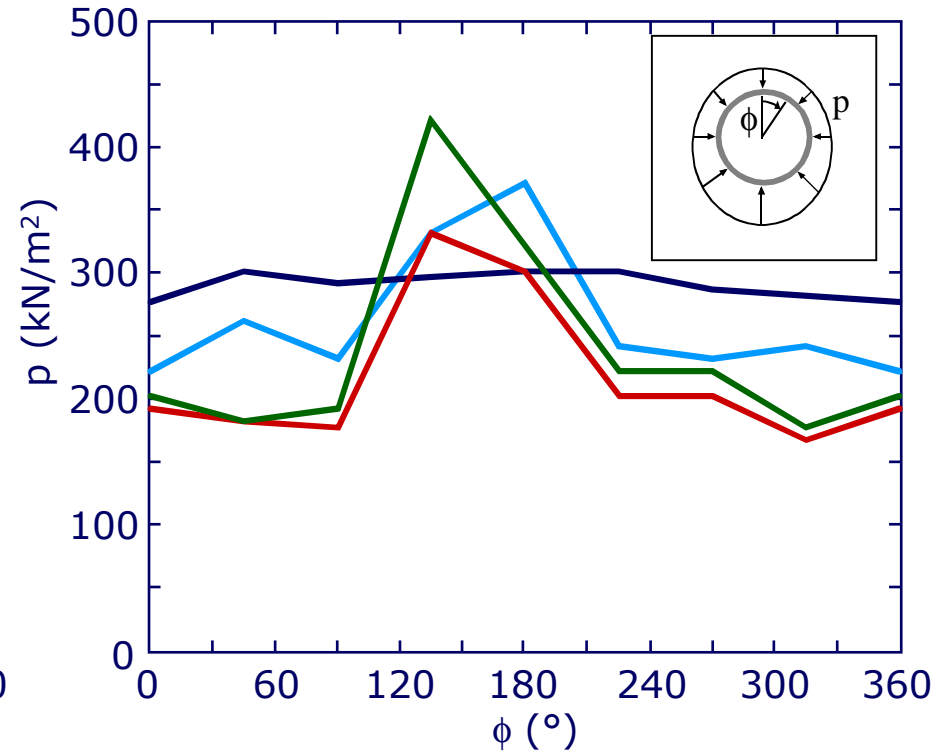


Computed lining pressure in the monitoring section



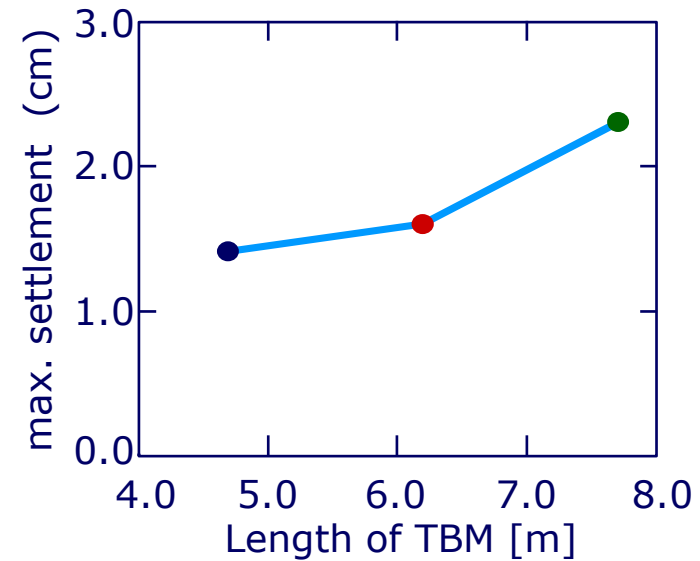
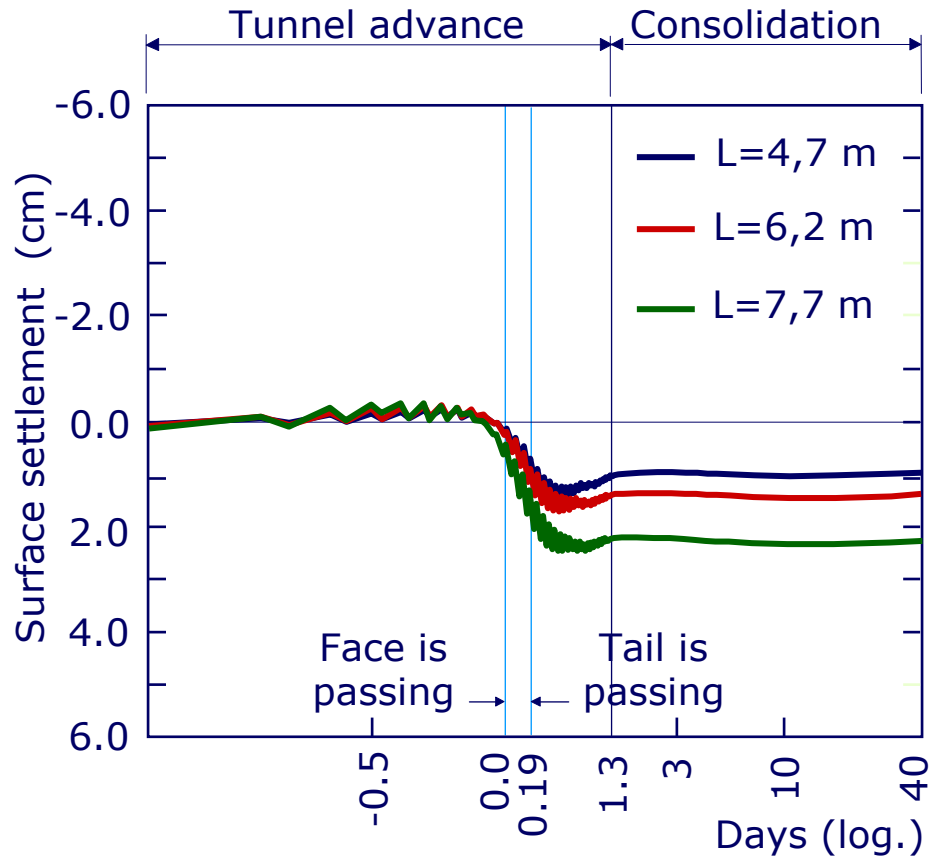
- At TBM tail
- 27 m behind shield $t = \infty$
- 5 lining rings behind shield
- Initial earth and pore pressure

Measured lining pressure on a tunnel in Japan [HASHIMOTO 2002]



- At TBM tail
- 1 month after passing of tail
- 5 lining rings behind shield
- 6 months after Passing of tail

Geometry-related parameters: Influence of length of TBM



Influence on surface settlements

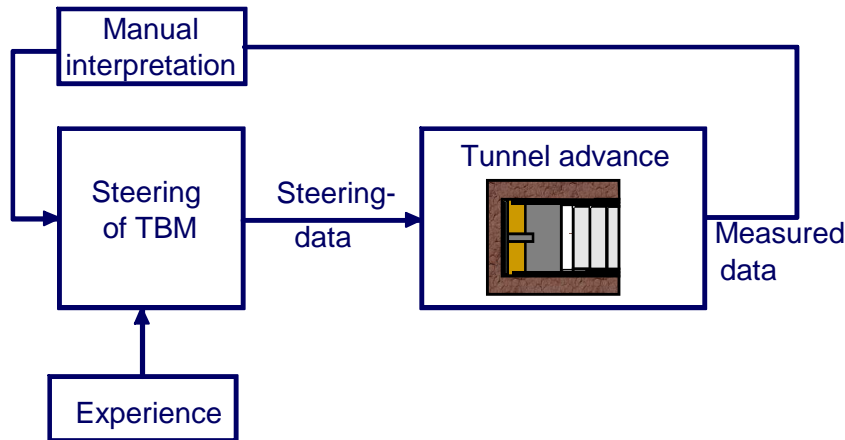
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Decision Support System for steering of TBM's

- Support of tunnel excavation by means of information and process management system
- Integration of numerical simulation and Methods of Computational Intelligence in real time

Current state



Mid-term perspective

